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SHAKER MILL POND DAM
MA 00732

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

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DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS. 02154

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JULY 1979

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HOUSATONIC RIVER BASIN WEST STOCKBRIDGE, MASSACHUSETTS

SHAKER MILL POND DAM MA 00732

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

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DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS. 02154

JULY 1979

PHASE I INVESTIGATION REPORT NATIONAL DAM INSPECTION PROGRAM

Identification No.: MA 00732

Name of Dam: Shaker Mill Pond Town: West Stockbridge

County: Berkshire
State: Massachusetts
Stream: Williams River
Date of Site Visit: 30 May 1979

BRIEF ASSESSMENT

Shaker Mill Pond Dam consists of a gunite covered concrete and masonry spillway structure between approach channel walls and abutting earth roadway embankments. The overall length of the dam is about 50 ft. and its maximum height is 20.4 ft. There are two regulating outlets at the dam site. The dam was originally built in 1910 to provide a pond for power generation. Shaker Mill Pond is now used for recreation and as a fire protection supply.

Due to extent of downstream development that would be affected in the event the dam were to fail, Shaker Mill Pond Dam is confirmed as having a "high" hazard potential in accordance with Corps of Engineers guidelines.

The dam is in fair condition, based on a visual examination of the structure. Several deficiencies, mainly due to deterioration, were noted. However, there was no evidence of settlement, lateral movement or other signs of structural failure of the dam, or other conditions which would warrant urgent remedial action.

Based on the "intermediate" size and "high" hazard potential classifications in accordance with Corps of Engineers guidelines, the test flood for this dam is the Probable Maximum Flood (PMF). Hydraulic analyses indicate that the test flood outflow of 27,200 cfs (inflow 40,500 cfs or 1,250 csm) would overtop the dam by about 18 ft. With the water level at the top of dam (level of Route 102 bridge deck), the ungated spillway capacity is approximately 1,600 cfs, which is 6 percent of the test flood outflow.

The Town of West Stockbridge, owner of the dam, should engage a registered professional engineer to 1) perform a detailed examination of the spillway under no flow conditions, 2) observe the owner demonstrate the operation of the outlet works, 3) investigate the seepage occurring at the abutments and 4) perform a more detailed hydrologic analysis and then investigate spillway discharge adequacy, as outlined in Section 7.2.

Any necessary modifications resulting from the investigations, and remedial measures, including repairing eroded and cracked portions of the dam, repairing the collapsed right discharge channel wall, rebuilding and restoring power to the gate house, removing debris in the downstream channel and sealing leaks through the outlet works, as outlined in Section 7.3, should be implemented by the Owner within one year after receipt of this report. The Owner should also prepare a formal operations and maintenance manual for the dam and establish an emergency preparedness plan.

ALDRICH. JR

HALEY & ALDRICH, INC. by:

Harl Aldrich President

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the office of Chief of Engineers, Washington, DC 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I Investigations are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the test flood is based on the estimated "probable maximum flood" for the region (greatest reasonably possible storm run-off), or a fraction thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential. Consideration of downstream flooding other than in the event of a dam failure is beyond the scope of this investigation.

The Phase I Investigation does <u>not</u> include an assessment of the need for fences, gates, <u>no-trespassing signs</u>, repairs to existing fences and railings and other items which may be needed to minimize trespass and provide greater security for the facility and safety to the public. An evaluation of the project for compliance with OSHA rules and regulations is also excluded.

TABLE OF CONTENTS

Section	Page
LETTER OF TRANSMITTAL	
BRIEF ASSESSMENT	
REVIEW BOARD PAGE	
PREFACE	i
TABLE OF CONTENTS	iii
OVERVIEW PHOTO	vi
LOCATION MAP	vii
1. PROJECT INFORMATION	
1.1 General	1
a. Authorityb. Purpose of Inspection	1
1.2 Description of Project	2
 a. Location b. Description of Dam and Appurtenances c. Size Classification d. Hazard Classification e. Ownership f. Operator g. Purpose of Dam h. Design and Construction History i. Normal Operational Procedures 	2 2 3 3 3 4 4 4
1.3 Pertinent Data	4
2. ENGINEERING DATA	
2.1 Design Data	9
2.2 Construction Data	9
2.3 Operation Data	9
2.4 Evaluation of Data	9

TABLE OF CONTENTS (Continued)

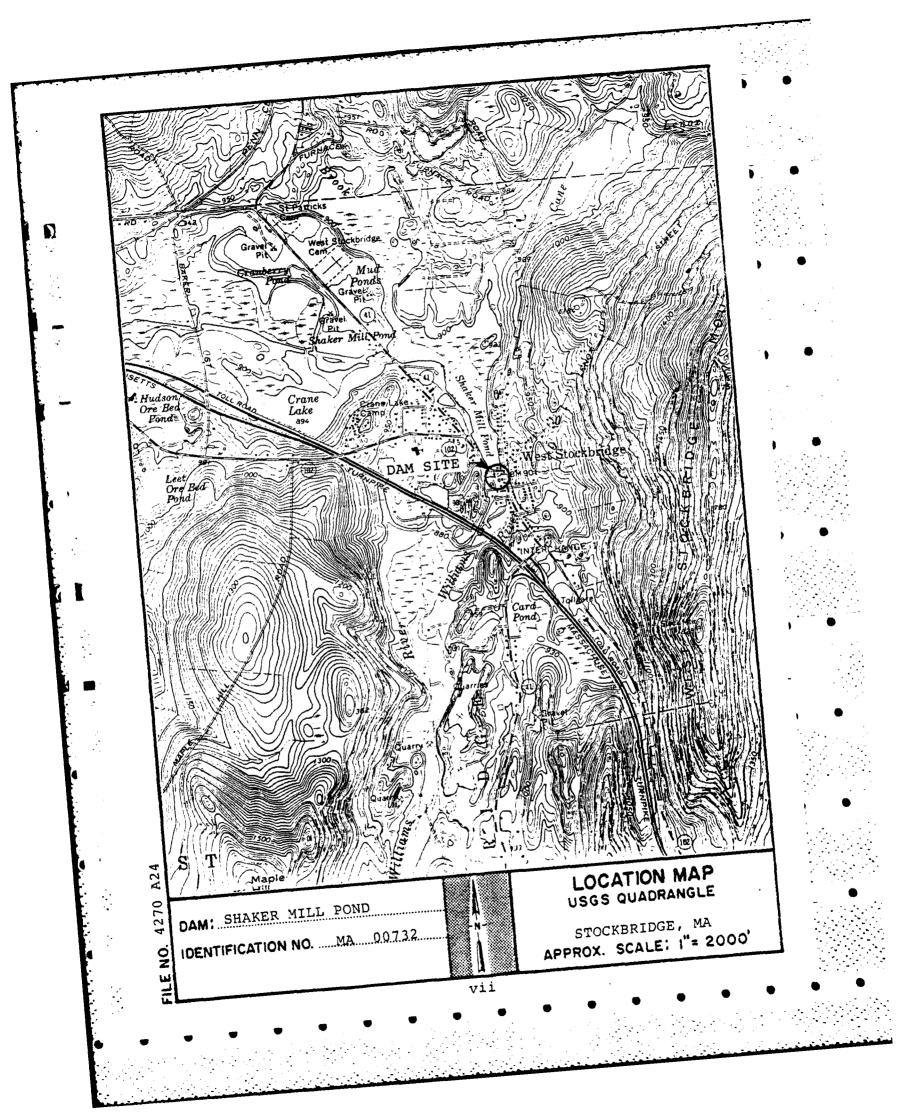
a. General b. Dam c. Appurtenant Structures d. Reservoir Area e. Downstream Channel 3.2 Evaluation 4. OPERATIONAL PROCEDURES 4.1 Procedures 4.2 Maintenance of Dam 4.3 Maintenance of Operating Facilities 4.4 Description of any Warning System in Effect 4.5 Evaluation 5. HYDRAULIC/HYDROLOGIC 5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	ige
a. General b. Dam c. Appurtenant Structures d. Reservoir Area e. Downstream Channel 3.2 Evaluation 4. OPERATIONAL PROCEDURES 4.1 Procedures 4.2 Maintenance of Dam 4.3 Maintenance of Operating Facilities 4.4 Description of any Warning System in Effect 4.5 Evaluation 5. HYDRAULIC/HYDROLOGIC 5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	
b. Dam c. Appurtenant Structures d. Reservoir Area e. Downstream Channel 3.2 Evaluation 4. OPERATIONAL PROCEDURES 4.1 Procedures 4.2 Maintenance of Dam 4.3 Maintenance of Operating Facilities 4.4 Description of any Warning System in Effect 4.5 Evaluation 5. HYDRAULIC/HYDROLOGIC 5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	.0
4. OPERATIONAL PROCEDURES 4.1 Procedures 4.2 Maintenance of Dam 4.3 Maintenance of Operating Facilities 4.4 Description of any Warning System in Effect 4.5 Evaluation 5. HYDRAULIC/HYDROLOGIC 5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	.0 .0 .1 .2
4.1 Procedures 4.2 Maintenance of Dam 4.3 Maintenance of Operating Facilities 4.4 Description of any Warning System in Effect 4.5 Evaluation 5. HYDRAULIC/HYDROLOGIC 5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	.3
4.2 Maintenance of Dam 4.3 Maintenance of Operating Facilities 4.4 Description of any Warning System in Effect 4.5 Evaluation 5. HYDRAULIC/HYDROLOGIC 5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	
4.3 Maintenance of Operating Facilities 4.4 Description of any Warning System in Effect 4.5 Evaluation 5. HYDRAULIC/HYDROLOGIC 5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	.5
4.4 Description of any Warning System in Effect 4.5 Evaluation 5. HYDRAULIC/HYDROLOGIC 5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	.5
Effect 4.5 Evaluation 5. HYDRAULIC/HYDROLOGIC 5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	.5
5. HYDRAULIC/HYDROLOGIC 5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	.5
5.1 Evaluation of Features a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	.5
a. General b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	
b. Design Data c. Experience Data d. Visual Observations e. Test Flood Analysis	.7
f. Dam Failure Analysis	.7 .7 .7 .7 .8
6. STRUCTURAL STABILITY	
6.1 Evaluation of Structural Stability	0
b. Design and Construction Data c. Operating Records d. Post-Construction Changes	0

TABLE OF CONTENTS (Continued)

Section	Page
7. ASSESSMENT, RECOMMENDATIONS AND REMEDIAL MEASURES	
7.1 Dam Assessment	21
a. Conditionb. Adequacy of Informationc. Urgencyd. Need for Additional Investigation	21 21 21 21
7.2 Recommendations	21
7.3 Remedial Measures	22
a. Operation and Maintenance Procedures	22
7.4 Alternatives	23
APPENDIX A - INSPECTION CHECKLIST	A-1
APPENDIX B - ENGINEERING DATA	B-1
APPENDIX C - PHOTOGRAPHS	C-1
APPENDIX D - HYDROLOGIC AND HYDRAULIC COMPUTATIONS	D-1
APPENDIX E - INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS	E-1



1. Overview of Shaker Mill Pond Dam



PHASE I INVESTIGATION REPORT NATIONAL DAM INSPECTION PROGRAM SHAKER MILL POND DAM MA 00732

SECTION 1 - PROJECT INFORMATION

1.1 General

a. Authority. Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region.

Haley & Aldrich, Inc. has been retained by the New England Division to inspect and report on selected dams in the State of Massachusetts. Authorization and notice to proceed were issued to Haley & Aldrich, Inc. under a letter dated 28 November 1978 from Colonel Max B. Scheider, Corps of Engineers. Contract No. DACW33-79-C-0018 has been assigned by the Corps of Engineers for this work. Camp, Dresser & McKee, Inc. was retained as consultant to Haley & Aldrich, Inc. on the structural, mechanical/electrical and hydraulic/hydrologic aspects of the Investigation.

- b. Purpose of Inspection. The primary purposes of the National Dam Inspection Program are to:
- 1. Perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.
- 2. Encourage and prepare the states to initiate effective dam safety programs for non-Federal dams.
- 3. Update, verify and complete the National Inventory of Dams.

1.2 Description of Project

- a. <u>Location</u>. Shaker Mill Pond Dam is located immediately downstream of the Route 102 bridge on Williams River near the center of West Stockbridge, Massachusetts, as shown on the Location Map, page vii. The latitude and longitude of the dam site are N42^O20.1' and W73^O22.1'. Williams River joins Housatonic River at a point about 8 miles south of the dam.
- b. Description of Dam and Appurtenances. Shaker Mill Pond Dam is approximately 50 ft. long and a maximum of 20.4 ft. in height. The dam itself consists of a concrete and masonry spillway weir immediately downstream of the concrete walls and earth embankments abuting the Route 102 bridge which form the approach channel to the spillway. Appurtenant to the dam are three outlets (two of which can be operated), a small wooden gate house, an abandoned generator structure and various concrete and stone masonry walls. The general configuration of the dam is shown on the "Site Plan Sketch", page C-1.

The main spillway is 20 ft. long, 1 ft. deep and ogee-shaped in cross-section, Photos No. 2 and 3. There are eight steel dowels on the main spillway crest (which is at El. 893.8 National Geodetic Vertical Datum (NGVD)) that could be used to install flashboards. The spillway length increases to about 50 ft. by stepped up sections on both sides of the main spillway, as shown on the overview photo and schematically on page D-7. The downstream face of the spillway and the adjacent training walls have been covered with gunite. The top of dam is considered to be the Route 102 bridge deck at El. 900.1.

The regulating outlets consist of two gated 36-in. diameter conduits. The outlet nearest the right (west) abutment has a manually-operated gate, Photo No. 4, and upstream invert at El. 887.5. The center outlet passing through the spillway is controlled by a motor-driven gate mechanism in the gate house above the spillway, Photo No. 3. Its upstream invert is at El. 889.0. There is also a gated conduit at the left (east) abutment of the spillway which was designed as a penstock to the turbine housed in a concrete generator structure at the spillway toe, Photo No. 9. However, this third

outlet is no longer operative.

The roadway embankments at the left and right abutments are approximately 30 ft. wide at the top of the dam and retained by concrete walls. There is also a 25 ft. long concrete wing wall through the right abutment parallel to the spillway axis. A 6-in. diameter pipe apparently drains the area behind the wall.

- c. Size Classification. Shaker Mill Pond Dam has an estimated maximum storage capacity of 1,200 acre-ft. at the top of dam. The corresponding maximum hydraulic height of the dam is 20.4 ft. Storage of from 1,000 to 50,000 acre-ft. classifies this dam in the "intermediate" size category, according to the guidelines established by the Corps of Engineers.
- d. <u>Hazard Classification</u>. Based on the Phase I investigations and dam failure analysis (Section 5.1f) in accordance with Corps of Engineers guidelines, Shaker Mill Pond Dam was found to have a "high" hazard potential. If the dam were to fail, a business and residential district along the river, particularly the right bank downstream of Depot Street, would be subject to serious flooding. Therefore, the potential for loss of lives and extensive economic loss to commercial and residential properties is high.
- e. Ownership. The name and address of the current owner is:

Board of Selectmen Town of West Stockbridge West Stockbridge, MA 01266

The Town of West Stockbridge reportedly acquired the dam from the Massachusetts Electric Company, Route 7, Great Barrington, MA in 1964. It was also reported that the South Berkshire Electric Power Company once owned the dam about twenty years ago (circa 1959), and that the original owner was Brossidy Mill (grist mill, circa 1895).

f. Operator. Mr. John Viola, Highway Superintendent,

Town of West Stockbridge, is responsible for operation, maintenance and safety of the dam. His office phone number is (413) 232-7794 and home phone number is (413) 232-7724.

- g. Purpose of Dam. The original purpose of the dam was to provide water power for a grist mill. A turbine and generator were installed at the dam site by a power company, but the equipment was never used to any extent. Currently the dam maintains the level of Shaker Mill Pond, which is used for recreation and as a fire protection supply.
- h. Design and Construction History. The dam was originally constructed in 1910. A drawing of the proposed dam by Barnes & Spaulding, Engineers, dated October 1909 is included in Appendix B. No further information regarding the original design and construction was disclosed.

In 1948 the bridge immediately upstream of the dam was overtopped in a flood, causing extensive damage to the dam and property in the center of town. Consequently the right abutment adjacent to the spillway was reconstructed, and a 20 ft. long section of the spillway was lowered by about 1 ft. to increase the discharge capacity.

It is not known when the generator structure was constructed at the toe of the spillway. In 1972 the Town of West Stockbridge completed extensive repairs to the dam to correct the unsafe conditions at the dam as directed by the Massachusetts Department of Public Works in a letter dated 16 June 1971 (see page B-4). The 1972 modifications may have included the gunite covering on the dam, constructing a buried cutoff wall upstream of the wing wall at the right abutment and a weep pipe to drain the area behind the wing wall.

i. Normal Operational Procedures. There is no formal established routine for the operation of the dam. The two regulating outlets are operated as required during periods of high water levels and heavy precipitation. Flashboards have not been installed at the dam for many years.

1.3 Pertinent Data

All elevations reported herein are approximate and

based on rough measurements made on 30 May 1979 at the dam site. The USGS benchmark on the left abutment of the Route 102 bridge, which is given as El. 901 NGVD, was used as the reference elevation.

Drainage Area. The total drainage area of Williams Brook above Shaker Mill Pond Dam shown on page D-1 is estimated to be 32.4 square miles. Ground elevations in the watershed vary from a low of about El. 900 near the dam to a high of about El. 2,070 on Pelly Peak in the Town of Richmond. The majority of the area consists of rolling woodland with some flat residential, swamp and pond areas.

Discharge at Dam Site

- 1. Outlet works..... a) 36-in. dia. waste outlet near right bank, Inv. El. 887.5 b) 36-in. dia. waste outlet through spillway, Inv. El. 889.0 c) Penstock to turbine (not operative)
- 2. Maximum known flood at dam site..... Not available

3. Ungated spillway capacity at top of dam

(without flashboards)... 1,600 cfs at El. 900.1

4. Ungated spillway capacity at test flood pool elevation (without

flashboards)........... 2,160 cfs at El. 918.0 (Portion of test flood flowing over spillway; the remaining 25,040 cfs would flow over the dam and banks)

5. Gated spillway capacity at normal pool elevation..... Not applicable

6. Gated spillway capacity at test flood pool elevation..... Not applicable

7. Total spillway capacity at test flood pool

elevation..... 2,160 cfs at El. 918.0 (see note for item 4)

	8. Total project discharge at test flood pool elevation	27,200 cfs at El. 918.0
c.	Elevation (ft. above NGVD)	
	 Streambed at centerline of dam	Unknown Not applicable 893.8 Not applicable 893.8 Unknown 900.1
d.	Reservoir .	
	 Length of maximum pool. Length of recreation pool. Length of flood control pool. 	1.0 mi. (Est.)
e. ·	Storage (acre-feet)	
	 Recreation pool Flood control pool Spillway crest Top of dam Test flood pool 	Not applicable 130 1,200
f.	Reservoir Surface (acres)	
	 Recreation pool Flood control pool Spillway crest Top of dam Test flood pool 	Not applicable 32 320

g. Dam

1.	Туре	Concrete and masonry gravity structure
2.	Length	
	Height	
	Top width	
	Side slopes	
6.	Zoning	Unknown
7.	Impervious core	Concrete and masonry walls
8.	Cutoff	Concrete and masonry
		walls
9.	Grout curtain	Unknown
10.	Other	Roadway embankment
		at each abutment has
		minimum 30 ft. width

h. Diversion and Regulating Tunnel. Not applicable

at top of dam

i. Spillway

1.	Type	Concrete and masonry gravity, overflow, ogee-shaped weir with no flashboards in place
2.	Length of weir	
	Crest elevation	
4.	Gates	None
5.	U/S Channel	wide by 9.5 ft. high
		opening under Route 102 bridge
6.	D/S channel	About 35 ft. wide with
		stone sidewalls; flow was slightly turbulent
7.	General	Several dwellings were built right on edge of the river bank

j. Regulating Outlets. There are two (2) regulating outlets for this dam. One 36-in. diameter pipe in the outlet works on the right has an invert of about El. 887.5 and is controlled through a hand-operated 42-in. square steel slide gate on the downstream side of the dam. The

second outlet is a 36-in. diameter pipe which passes through the spillway to the left of the outlet structure and has an invert of about El. 889.0. The 4-ft. square wooden gate for this pipe is operated through gearwheels activated by a motor driven belt wheel located in a small wooden gatehouse above the spillway. There was no belt on the wheel at the time of the site visit (30 May 1979). Furthermore, there is no electrical power source to the gatehouse, so electrical power for the motor must be taken from the adjacent Shaker Mill Museum. In the event power is not available, a handle on the belt wheel can be used to manually operate the gate.

The penstock to the turbine in the generator structure at the toe of the spillway on the left side is controlled by a wooden gate on the upstream side which is inoperative.

SECTION 2 - ENGINEERING DATA

2.1 Design Data

One drawing of the proposed dam dated 1909 is available.

2.2 Construction Data

No engineering data documenting the original construction of the dam are available. The post-construction changes described in Section 1.2h are based on information contained in prior inspection reports or reported by the operator of the dam, Mr. John Viola.

2.3 Operation Data

Prior county and state inspection reports since 1968 are the only operation records available for this dam.

2.4 Evaluation of Data

- a. Availability. A list of the limited quantity of engineering data available for use in preparing this report is included on page B-1. Documents from the listing are also included in Appendix B.
- b. Adequacy. There was a lack of engineering data available to aid in the evaluation of Shaker Mill Pond Dam. This Phase I assessment was therefore based primarily on visual examination, preliminary hydraulic and hydrologic computations, consideration of past performance and application of engineering judgement.
- c. Validity. The information contained in the engineering data may generally be considered valid. However, the dimensions of the dam given in the 18 January 1973 state inspection report, page B-11, differ somewhat but not significantly from those measured on 30 May 1979 during the Phase I site visit.

SECTION 3 - VISUAL EXAMINATION

3.1 Findings

a. General. The Phase I visual examination of Shaker Mill Pond Dam was conducted on 30 May 1979. The upstream water surface elevation was about 0.7 ft. above the 20 ft. long spillway crest or El. 894.5 NGVD on that day.

In general, the project was found to be in fair condition. Several deficiencies which require correction were noted.

A visual inspection check list is included in Appendix A and selected photographs of the project are given in Appendix C. A "Site Plan Sketch", page C-1, shows the direction of view for each photograph.

b. Dam. The dam is basically an ogee-shaped spillway between concrete or stone masonry side walls, Photos No. 1, 2 and 3. Gunite had been applied to the downstream face of the spillway and is now cracked and separated from the spillway in several locations. Although the downstream face is partially obscured by flowing water, the location of the principal crack or cracks is evident where water impinges on the displacement at the crack, Photo No. 3. Large pieces of gunite have broken off above and below the center outlet pipe and surface erosion is evident in many areas of the irregular downstream face of the spill-way.

Large portions of gunite covering have broken off the left downstream training wall of the right outlet works structure, revealing a concrete wall with several cracks and heavy surface erosion, Photo No. 5. The downstream face of the outlet structure under the wooden operating platform is constructed of grouted stone masonry in fair condition. The remaining concrete portions of the outlet structure and exposed portion of the concrete wing wall are in good condition, Photo No. 4. Note that a 6-in. diameter pipe is flowing about one-third to one-half full,

Photo No. 4, apparently draining an area immediately behind the wing wall.

Seepage is occurring through some broken rock fill at the right (west) abutment, Photos No. 4 and 10, emerging about 1 ft. above the tailwater elevation or 8.5 ft. below the upstream pond level. The water is clear with no evidence of turbidity. Seepage is also occurring at the toe of broken rock fill at the left (east) abutment, Photo No. 8, at an elevation approximately 3 ft. below the upstream pond level. The estimated flow from this spring is about 2 to 3 gallons per minute. The water appeared to be clear.

c. Appurtenant Structures. The approach channel is formed by two walls (downstream of the concrete abutments of the Route 102 bridge shown on Photo No. 12). The right (west) concrete wall was reportedly built in 1948. It appears to be in good condition, except for a large horizontal crack or deteriorated joint near the water line, Photo No. 2, through which seepage occurring at the downstream end of the right abutment may be entering. The short left (east) wall appears to be stone masonry construction covered with gunite, Photo No. 6. It was wet at the contact between the gunite covering and the left abutment, Photo No. 8, where seepage was observed.

An outlet works structure is present between the spillway weir and the right discharge channel wall, Photo No. 4. The operating platform for the slide gate control is constructed of wood and is in good condition. The support for the platform is adequate. The wooden walkway ramp to the platform is on a steep grade and could be slippery during bad weather. There are no handrails on the platform or the walkway ramp. The outlet conduit is controlled by a manually operated steel slide gate, partially shown on Photo No. 5, which was reported to be operational, but was not opened during the site visit. The closed gate is leaking.

The wooden gate structure to the left of the outlet works, Photos No. 1, 2, 3, 6 and 11, is used to house control mechanism for the 36-in. diameter

pipe which discharges on the downstream face of the spillway. The structure is in very poor condition. The windows are broken, and the floor is badly deteriorated. There is no easy access to the gate-house from the adjacent concrete platform nor are handrails provided for safety. The control mechanisms are gearwheels activated by a motor driven belt wheel, Photo No. 7. However, no belt was observed and there was no electrical power source to the gatehouse. It was reported that the only power near the dam which could be used was in Shaker Mill Museum. The gate control mechanism could also be operated manually. The gate was fully open during the site visit, Photo No. 3.

On the left (east) side of the spillway at the toe of the dam is an abandoned concrete structure which houses a turbine and generator, Photos No. 1, 6, 9 and 11. The walls of the structure are stained and show several cracks with efflorescence. The flow to the generator structure was controlled by a wooden gate operated through a wooden stem rack and pinion gear device, Photos No. 2 and 6. The gate is not operative. A hole was broken out on the downstream wall of the generator structure to allow the water seeping through the gate to return to the downstream channel, Photo No. 9.

The left (east) discharge channel wall is of grouted stone masonry construction and appears to be in relatively good condition, Photo No. 9. The right (west) wall is of similar construction and for the most part is also in relatively good condition. However, the first 20 ft. of the wall beyond the dam appear to have experienced a structural failure, and some of the remains are seen in the channel, Photo No. 10. Water was observed seeping through the left abutment at this location.

d. Reservoir Area. Shaker Mill Pond is a relatively long, shallow reservoir, Photo No. 13. There are flat residential areas on either side of the pond immediately upstream of the dam. The shoreline to the north consists generally of wooded slopes and swampy areas. There is no significant probability of landslides into the reservoir affecting the safety of the dam.

Sedimentation has raised the pond bottom to about El. 887 upstream of the dam, which is 5 to 7 ft. higher than the downstream channel bottom just below the dam.

e. Downstream Channel. Williams River joins the Housatonic River at a point about 8 miles south of West Stockbridge. About 1,600 ft. downstream from the dam the river passes under the Massachusetts Turnpike. A 1,000 ft. long channel portion immediately downstream of the dam and within the downtown area of West Stockbridge was studied for flood impacts. Within this area there are commercial and residential type buildings on both banks of the channel.

The channel, in general, has a rectangular shape with bottom widths varying from 35 to 50 ft. and depths varying from 10 to 15 ft. at the banks. Erosion protection of both banks is provided by stone masonry walls. The left bank, where Route 102 is located, is relatively higher than the right bank.

The first bridge over the channel is on Depot Street, about 300 ft. downstream from the dam. It is a concrete bridge with a rectangular opening 38.5 ft. wide and 13.3 ft. high. Edges of foundation walls under several buildings are flush with the channel sidewalls. The land level on the right bank drops by about 5 ft. at a distance of about 50 ft. below the bridge. Another bridge is located about 200 ft. downstream from Depot Street. The rectangular clear opening under this bridge is 40 ft. wide and 7.8 ft. high. The channel bottom slope is controlled with an existing shallow overflow weir about 250 ft. below the second bridge.

3.2 Evaluation

Based on the visual examination conducted on 30 May 1979, Shaker Mill Pond Dam is considered to be in fair condition. Although the dam showed no signs of instability during the site visit, the fair condition assessment is due to the general deterioration of the gunite and concrete, the deteriorated conditions of the wooden gate structure, the lack of power at the gate structure, and the condition of the right channel wall downstream of the dam. Seepage is also occurring at both abutments of the

of the dam, which was noted by the Massachusetts Department of Public Works in 1971 in a list of several unsafe conditions at the dam requiring prompt action. Evidently, the remedial measures taken in 1972 by the owner did not eliminate the seepage entirely.

SECTION 4 - OPERATIONAL PROCEDURES

4.1 Procedures

In general, there are no formal procedures to provide routine maintenance and satisfactory operation of the dam. The two regulating outlets are operated as required during periods of high water and heavy precipitation. Flashboards are generally not installed at the spillway.

4.2 Maintenance of Dam

There are no established procedures or manuals for inspection and maintenance of the dam. No maintenance work on the dam has reportedly been performed since the extensive 1972 repairs requested by the Massachusetts Department of Public Works in 1971.

4.3 Maintenance of Operating Facilities

It was reported that the operating facilities are maintained on a demand basis. Although the gate mechanisms appear to be well maintained, the condition of the wooden gatehouse indicates that this facility, in general, has received little or no maintenance for sometime. The left (east) outlet gate was replaced and a new platform constructed over the right (west) outlet gate in 1960, according to the 1968 state inspection report.

4.4 Description of any Warning System in Effect

There is no warning system or emergency preparedness plan in effect for this structure.

4.5 Evaluation

The owner should prepare an operations and maintenance manual for the dam. The manual should delineate the routine operational procedures and maintenance work to be done on the dam to provide satisfactory operation and minimize deterioration of the facility. For example, an annual observation and maintenance program should be established to examine the dam and maintain outlets,

walls and channels. Incorporated in this procedure should be a procedure to operate the reservoir outlet gates periodically.

Since failure of the dam would probably cause loss of life and extensive property damage downstream, the owner should also prepare and implement a formal emergency preparedness plan and warning system.

SECTION 5 - HYDRAULIC/HYDROLOGIC

5.1 Evaluation of Features

- a. General. The dam consists of a concrete and masonry spillway between approach channel walls and earth abutments. The bridge on Route 102 is immediately upstream of the dam, and this structure would control major discharges from the reservoir. The original purpose of the dam was to provide water storage and flow regulation for power generation at the dam site. Now the pond is mainly used for recreational purposes.
- b. Design Data. No original hydrologic or hydraulic design data were available for this dam site.
- c. Experience Data. No historical records of the maximum flows are available. However, reportedly, Route 102 was overtopped and several dwellings downstream from the dam were flooded during the 1948 flood. The spillway crest was lowered by one foot and the right abutment was reconstructed with concrete after the flooding event.
- d. Visual Observations. Shaker Mill Pond at normal levels has an average width of about 300 ft. and a length of about 1 mile. It is surrounded by rolling woodlands. On the day of the site visit, 30 May 1979, about 0.7 ft. of water was flowing over the spillway, which had no flashboards. The depth of the pond, just upstream of the spillway, was measured at about 8.0 ft. The center outlet underneath a small gate house was fully open. A gate on the right (west) outlet was closed. The left (east) outlet which was used to convey flows into the generator structure was permanently blocked.

Medium size trees and bushes were observed on the sides of the channel, particularly within the section between the dam and Depot Street. Several dwellings were either at the flood plain or extended right on top of the channel side wall. Two bridge crossings exist over the channel within a distance of about 500 ft. from the dam. Vertical side walls of the channels are made of stone masonry.

The main spillway crest is 20 ft. long and 1 ft. deep. The length increases to about 50 ft. by stepped up sections on both sides of the main spillway (page D-7). A bench mark with elevation 901.0 is located on top of the Route 102 bridge left abutment wall.

e. <u>Test Flood Analysis</u>. Based upon the Corps of Engineers guidelines, the recommended test flood for "intermediate" size dams having a "high" hazard potential is the PMF (Probable Maximum Flood). The PMF was determined using Corps of Engineers Guidelines for Estimating Maximum Probable Discharge in the Phase I Safety Investigation. The watershed terrain was determined to be 95 percent rolling and 5 percent flat (swamp and water surface). From this, an inflow rate of 1,250 cfs per square mile (csm) was interpolated for the drainage area of 32.4 square miles. The resulting PMF inflow is 40,500 cfs.

Surcharge-storage routing was performed through Shaker Mill Pond using the stage-discharge and area-volume curves shown in Appendix D. Flow through the low-level outlet conduits were ignored for this evaluation. The test flood outflow, estimated to be 27,200 cfs, would occur when the water surface elevation in the pond is at El. 918.0. This is about 18 ft. above the top of the dam. At this time the tail water elevation would be about 12 ft. above the river banks. As a result, a large area extending from upstream to downstream of the dam would be seriously flooded.

With the water level at the top of dam, the capacity of the existing spillway at this dam site is about 1,600 cfs or 6 percent of the test flood outflow. There is therefore a high probability of the dam (Route 102 roadway) being overtopped.

f. Dam Failure Analysis. Based on Corps of Engineers Guidelines for Estimating Dam Failure Hydrographs, and assuming that a failure would occur along 85 percent of the spillway structure, the peak failure outflow is estimated to be 6,470 cfs. The flow just before failure would be approximately 1,600 cfs. As shown in Appendix D, the hydraulic profile for a discharge of 1,600 cfs would be below the top of the lower bank. Because of this prior condition, the

failure could occur with people in the flood hazard area unprepared.

The storage capacity of the downstream channel within the study area is negligible in comparison to the volume of the pond prior to the failure. An approximate failure flood hydraulic profile is shown on page D-9, Appendix D. The area extending about 200 ft. downstream from Depot Street, particularly on the right bank, would be subject to a serious flooding. Here a hardware store, three two-story commercial and residential buildings on Depot Street, another residential building, one exhibit hall, and one restaurant - resident complex on the lower area downstream of Depot Street are estimated to be subject to flooding to a depth varying from 4 ft. to 7 ft.

In conclusion, in the event of a dam failure, potential for loss of lives exists and excessive residential and commercial property damages are expected to occur. Therefore, the hazard potential classification for this dam is considered high, in accordance with Corps of Engineers guidelines.

SECTION 6 - STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

- a. <u>Visual Observations</u>. There was no visual evidence of dam instability during the site visit on 30 May 1979. There was no evidence of movement of structural items, except for the collapsed section of the downstream channel wall to the right of the dam.
- b. Design and Construction Data. Design data in the form of a drawing of the original proposed dam construction (dated 1909) is available. Review of the drawing indicates that the dimensions and configuration of the spillway is consistent with typical spillways of this magnitude.
- c. Operating Records. There were no known operating records available for this facility to aid in the evaluation of the structural stability.
- d. Post-Construction Changes. Review of the drawing of the original proposed dam construction, the different methods of construction and different shades and consistencies of concrete indicate that this dam has been repaired and altered several times. During the site visit, it was reported that the right outlet structure has been reconstructed, the main spillway crest lowered and a cut off wall added to the right of the outlet.
- e. <u>Seismic Stability</u>. Shaker Mill Pond Dam is located in a Seismic Zone l and in accordance with Recommended Phase I Guidelines does not warrant seismic analysis.

SECTION 7 - ASSESSMENT, RECOMMENDATIONS AND REMEDIAL MEASURES

7.1 Dam Assessment

a. Condition. The visual examination of Shaker Mill Pond Dam revealed that the structure was in fair condition. Although there were no signs of impending structural failure or other conditions which would warrant urgent remedial action, several deficiencies were noted.

Based on the results of computations included in Appendix D and described in Section 5, the spillway is not capable of passing the test flood, which for this structure is the PMF. The test flood outflow of 27,200 cfs (inflow 40,500 cfs or 1,250 csm) would overtop the dam by about 18 ft. With the water level at the top of dam, the spillway capacity is about 1,600 cfs, which is 6 percent of the test flood outflow.

- b. Adequacy of Information. This evaluation of the dam is based primarily on visual examination, preliminary hydraulic and hydrologic computations, consideration of past performance and application of engineering judgement. Generally the information available or obtained was adequate for the purposes of a Phase I assessment. However, it is recommended that additional information regarding the configuration of the dam, its structural stability and the seepage occurring at the abutments be obtained, as outlined in Section 7.2.
- c. <u>Urgency</u>. The recommendations for additional investigations and remedial measures outlined in Section 7.2 and 7.3, respectively, should be undertaken by the Owner and completed within one year after receipt of this report.
- d. Need for Additional Investigation. Additional investigations should be performed by the Owner as outlined in Section 7.2.

7.2 Recommendations

It is recommended that the Town of West Stockbridge,

owner of the dam, engage a registered professional engineer to undertake the following investigations:

- 1. Perform a detailed inspection of the spillway during no or low flow conditions.
- Observe the owner demonstrate the operation of the outlet works slide gate to the right of the spillway and the gate control mechanism for the outlet through the spillway.
- 3. Perform an investigation to evaluate the seeping that is occuring through the right and left channel walls downstream of the dam. The investigation should include a comparison of the location, character and amount of seepage flow at times of high and low pond levels in an effort to determine the paths of seepage.
- 4. Perform a more detailed hydrologic analysis.

 Based on the findings, investigate spillway discharge adequacy.

The Owner should then implement corrective measures on the basis of these engineering investigations.

7.3 Remedial Measures

The dam is generally in fair to poor condition, and it is considered important that the following items be accomplished:

- a. Operation and Maintenance Procedures. The following should be undertaken by the Owner:
 - 1. Repair erosion damage to the dam in general. The repairs should include the removal of all the gunite and provide erosion protection which would be more resistant to the type of conditions which this dam experiences.
 - 2. Repair the large horizontal crack or deteriorated joint in the right (west) approach channel wall.
 - 3. Reconstruct the stone masonry wall where it has collapsed on the right side downstream of the dam.

- 4. Remove the debris in the channel downstream of the outlet structure.
- 5. Reconstruct the wooden gatehouse and supply electrical power for the operation of the gate.
- 6. Seal off the inlet to the abandoned generator structure and repair the leaking steel gate for the right outlet works.
- 7. Prepare an operations and maintenance manual for the dam. The manual should include provisions for annual technical inspection of the dam and for surveillance of the dam during periods of heavy precipitation and high reservoir water levels. The procedures should delineate the routine operational procedures and maintenance work to be done on the dam to ensure satisfactory operation and to minimize deterioration of the facility. The regulating outlet gates should be operated periodically.
- 8. Develop a written emergency preparedness plan and warning system to be used in the event of impending failure of the dam or other emergency conditions. The plan should be developed in cooperation with local officials and downstream inhabitants.

7.4 Alternatives

In addition to sealing off the inlet to the generator structure, the structure should be demolished and removed, thus eliminating a large obstruction to flow over the spillway during high water flow.

APPENDIX A - INSPECTION CHECK LIST

	Page
VISUAL INSPECTION PARTY ORGANIZATION	A-1
VISUAL INSPECTION CHECK LIST	
Dam Abutments and Roadway Embankment	A-2
Outlet Works - Spillway Weir, Approach and Discharge Channels	A-3
Right Outlet Works	A-4
Outlet Works - Gate House	A-5
Congrator Structure	2-5

VISUAL INSPECTION PARTY ORGANIZATION NATIONAL DAM INSPECTION PROGRAM

Dam: Shaker Mill Pond

Date: 30 May 1979

Time: 1030-1300

Weather: Overcast with light rain, temperature 60's F.

Water Surface Elevation Upstream: El. 894.5 NGVD (0.7 ft.

above top of concrete

weir)

Stream Flow: Estimated 50 cfs

Inspection Party:

Harl P. Aldrich, Jr. - Soils/Geology

Richard A. Brown

Haley & Aldrich, Inc.

A. Ulvi Gulbey - Hydraulic/Hydrologic

Robert H. Sheldon

Robert P. Howard - Structural/Mechanical

Camp, Dresser & McKee, Inc.

Present During Inspection:

John Viola, Highway Superintendent, Town of West Stockbridge

DAM: Shaker Mill Pond DATE: 30 May 79

	* ************************************
AREA EVALUATED	CONDITION
DAM ABUTMENTS AND ROADWAY EMBANKMENT	
Crest Elevation	Top of dam considered to be level of Route 102 bridge deck, El. 900.1 NGVD
Current Pool Elevation	E1. 894.5, 0.7 ft. above the main spillway crest
Maximum Impoundment to Date	Unknown
Surface Cracks	None observed
Pavement Condition	Good on Route 102 roadway
Movement or Settlement of Crest	None evident
Lateral Movement	None evident
Vertical Alignment	Good
Horizontal Alignment	Good
Condition at Abutment and at Concrete Structures	Concrete left bridge abutment cracked; large horizontal crack in right approach channel wall near upstream water level
Indications of Movement of Structural Items on Slopes	None observed
Trespassing on Slopes Animal Burrows in Embank- ment	Unrestricted None observed
Vegetation on Embankment	Minor vegetation in rock fill on downstream side of abutments
Sloughing or Erosion of Slopes or Abutments	Erosion on downstream side of right abutment due to collapse of down-stream channel wall
Rock Slope Protection - Riprap Failures	Concrete wall on upstream side of roadway. Broken rock fill on down-stream side of abutments
Unusual Movement or Cracking at or near Toes	None observed
Unusual Embankment or Downstream Seepage	Clear water seeping through broken rock fill on downstream side at both abutments (Emerging 1 ft. above tailwater on right side; 2-3 gpm about 3 ft. below pond level on left side)
	A-2

DAM: Shaker Mill Pond DATE: 30 May 79

AREA EVALUATED	CONDITION
THE EVACORIES	3011011
Piping or Boils Foundation Drainage Features	None observed, seepage clear None known to exist
Toe Drains	6-in. pipe flowing one-half to one- third full draining area behind wing wall at right abutment
Instrumentation Systems	None
OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DIS- CHARGE CHANNELS	
a. <u>Approach Channel</u>	
General Condition	Right concrete wall is in good con- dition, except for a large horizont- al crack or deteriorated joint near the water surface level. Left wall appears to be stone masonry with gunite coating in good condition
Loose Rock Overhanging Channel	None observed
Trees Overhanging Channel	None observed
Floor of Approach Channel	Submerged - not observed
b. Weir and Training Walls	
General Condition of Concrete	General condition is fair
Rusting or Staining Spalling	Some rusting and staining observed Gunite covering over major portion of the dam cracked and separated from dam surface. Large pieces of gunite broken off in several locations
Any Visible Reinforcing	
	A-3

HALEY & ALDRICH, INC. CAMBRIDGE, MASSACHUSETT

DAM: Shaker Mill Pond DATE: 30 May 79

AREA EVALUATED	CONDITION
AREA EVALUATED	CONDITION
Any Seepage or Efflo- rescence	Minor efflorescence observed
Drain Holes	None observed
c. <u>Discharge Channel</u>	
General Condition Loose Rock Overhanging Channel	General condition is good None observed
Trees Overhanging Channel	None observed
Floor of Channel Walls	Submerged - not observed Left wall is grouted stone masonry in good condition. Right wall is grouted stone masonry, and for the most part in good condition. 15 to 20 ft. of wall downstream of dam has failed and some remains in channel
RIGHT OUTLET WORKS	
General Condition Training Wall	General condition is good to fair Concrete wall covered with gunite. Large areas of gunite spalled off. Cracks in wall with heavy surface erosion
Outlet Walls	Downstream face of outlet of grouted stone masonry in fair condition. Remaining portions of concrete construction in good condition. Concrete wing wall in good condition dition
Platform	Wood construction in good condition. Support of platform only adequate. Remains of old platform observed. Walkway of wood plank on steep grade. No handrails on platform or walkway
	A-4

DAM: Shaker Mill Pond DATE: 30 May 79

AREA EVALUATED	CONDITION
Gate	Manually operated slide gate in good condition. Gate leaking. Not operated during the investigation
OUTLET WORKS - GATE HOUSE	
a. <u>General Condition</u>	Wooden gate house in very poor con- dition. The windows are broken. Floor is in a very deteriorated condition
b. Mechanical and Electrical	
Float Wells Service Gate	None 36-in. diameter gate operated by gearwheels activated by a motor driven beltwheel in good condition. Provisions for manual operations provided. Belt not present
Lightning Protection System	None observed
Emergency Power System	Electric box and wiring observed, but no power line to gate house. Power must be brought in from Shaker Mill Museum
Wiring and Lighting System in Gate House	None observed
GENERATOR STRUCTURE	
General Condition of Concrete	General condition of concrete is good
Rust or Staining Spalling	Some rust and staining observed None observed
Visible Reinforcing Cracks Effloresence	Reinforcing exposed in discharge hole Several surface cracks observed Efflorescence observed at surface cracks
	A-5
HALEY & ALDRICH, INC.	

DAM: Shaker Mill Pond DATE: 30 May 79

AREA EVALUATED	CONDITION
Drain Holes	Drain hole broken out on downstream wall. Gate seepage runs out hole to channel
Gate .	Reported wooden gate with wooden stem rack and pinion gear device. Gate was leaking
Other	Water wheel extremely rusted and abandoned
•	
MALEY & ALORICH MIC	A-6

NO. 4150

HALEY & ALDRICH, INC. CAMBRIDGE MASSACHUSETTS

APPENDIX B - ENGINEERING DATA

		Page
LIST OF AVAILABLE DATA	<u>A</u>	B-1
PRIOR INSPECTION REPOR	RTS	
Date	By Whom	
12 August 1968	County of Berkshire	B-2
17 May 1971	Mass. Dept. of Public Works	B-3
16 June 1971 (letter)	Mass. Dept. of Public Works	B-4
18 January 1973	Mass. Dept. of Public Works	B-6
13 November 1974	Mass. Dept. of Public Works	B-12 '
4 November 1976	Mass. Dept. of Public Works	B-15
DRAWINGS	:	
"Proposed Dam at Shake Engineers, October 19	er Mill," Barnes & Spaulding, 909	B-19

LIST OF AVAILABLE DATA SHAKER MILL POND DAM

Location	Mass. Department of Environmental Quality Engineering, Division of Waterways, 100 Nashua Street, Boston, MA 02114 and page B-2	Mass. Department of Environmental Quality Engineering and pages B-3 through B-18	Berkshire County Engineering Department, Court House, Pittsfield, MA 01201 and pages B-19 and B-20
Content	Report dated 12 August 1968	Four reports from 1971 through 1976, including cover letters and description of dam, if any	Plans, sections, elevation and details of proposed dam, Scale: 1 in. = 4 ft.
Document	County inspection reports, Shaker Mill Pond Dam	State inspection reports, Dam No. 1-2-326-3	Drawing entitled "Proposed Dam at Shaker Mill" by Barnes & Spaulding, Engineers, October 1909

COUNTY OF BERKSHIRE, MASS. INSPECTION OF DAMS

	Nugue	12,1968	
Inspector	Willia	m A Heaph	Y
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INSPECTION OF DAYS

Page 129-3

REPLEMINE TO THE TOTAL TO THE T

Date ____May 17, 1971 City or Town of West Stockbridge Inspector R. Northrup & P. Fezzie Name of Dam Shaker Mill Owner Town of West Stockbridge Address Town Hall Caretaker Town of West Stockbridge Address Town Hall Location At center of village on Route 41 at bridge. Type of Dimensions Conc. gravity type roadway forms earth embank. 100' long, 14' high. and the contraction of the contr Spillway, type and size _Conc. 35' long, 4' freeboard. Westgate 42" square steel Center gate 4' square wood Outlets, type and size Eastgate to generator house 4 X 5 wood. Flashboards, type and height None - provisions made Condition Poor Date Built __ 1910 ____ Mhen last repaired 1960 By whose orders Owners Nature of Repairs East gate replanded, new platform over west gate. Purpose of Dam Formerly power. Approximate storage of water 65 acres Possible damage due to failure of dam Disastrous to Town. Remarks Water 10" over spillway. West gate leaking. Nest end at spillway leaking. badly. Seepage at east end. Center gate open. Recommendations Immediate repairs. 2 pictures taken. In medicate interes Notes Parketing County Earn Port : 14 11 12 1905 Letter to Pot of Solist a hora 14 1971

Juno 16, 1971

THEY WHENTER ADMINISTRA

Fourd of Calcatann Wast Stockbridge Massachusetts 01250

Gentlemen:

Res Shaker Mill - Dam

This office has been made aware of the unsele conditions of Shaker Mill Dam. Inspection reports by Berkshire County Engineer dated August 12, 1963 and the Department of Public Works dated May 17, 1971 point out the need for immediate repairs.

In accordance with Chapter 253 of the Massachusetts Coneral Laws, as most recently amended by Chap. 595 of the Acts of 1970, the Commissioner of the Massachusetts Department of Public Norks is responsible for inspection of the safety of mill dams and reservoirs and their potential hazards to life and property downstream.

Soction 46 of Chapter 595 provides that the Commissioner shall determine and direct what alterations and repairs are required to make the structure permanent and secure, and shall in writing order the owner thereof to make such alterations or repairs within a reasonable time.

based on the report of inspection, I find it necessary to inform you that the following deficiencies were found and that corrective measures should be initiated within (30) thirty thus from receipt of this letter.

Board of Selectmon, Stockbridge

June: 10, 1971

You are bereby directed to:

1. Control water over spillway.

2. Comis leaking west Case.

3. Repair looking spillway at West Indo-

4. Correct seepage at cast end.

5. Make center gate operative.

I sincerely hope that you will recognize your responsibility in this matter and make the necessary repairs
to render the dam safe.

Your groupt action in this matter would be appreciated.

Very truly yours,

ROBERT 5. FOSTER Acting Commissioner

c.c. Dist. #1

LBA: serm

LRA

Ec

1 -	Location: City/Town West Stockbridge	Dam No.	1-2-326-3	
••				
	Name of Dam Shaker M11		ed by: Rolondan	
		Date of	Inspection 1-18-7	3
2.,	Owner/s: per: Assessors	Prev.	nspectionX	
			• • •	
	Reg. of Deeds			
-	Town of West Stockbridge - West			
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	Name St. & No.	City/Town	State Tel	. No
3.	<u> </u>			
	Caretaker [if any] e.g. superintendent owner, appointed by multi owners. flame St. & He.	C1 cy/Tox:		
4.				
٠.	No. of Pictures taken2	••		
5.	No. of Pictures taken 2 Degree of Hazard: [if dam should fail	completely]*		
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5.	Degree of Hazard: [if dam should fail 1. Minor 3. Severe X *This rating may change as land use ch Outlet Control: Automatic Operative X Comments: Upstream Face of Dam: Condition:	2. ! 4. [anges [future o Fanual_ yes:	Disastrousisvelopment]	
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	A - 2 - DAM NO. 1-2-3:
e. Do	whistream Face of Dam: Condition: 1. Cood_X 2. Minor Repairs_
	3. Major Repairs 4. Urgent Repairs
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٠, , •	
- 	
Er	ergency Spillway: Condition: 1. Good 2. Minor Regairs
eimo ni anno e	3. Major Recajrs .4. Urgent Rcpairs
	Comments:
	principal spillway X.
-	principal spillway X
11. :	other
	mmary of Deficiencies Noted: Growth [Trues and Brush] on Embankment None Animal Burrows and Washouts Damage to slopes or top of dam Cracked or Damaged Masonry Evidence of Seepage Evidence of Piping Erosion Leaks
	other
	mmary of Deficiencies Noted: Growth [Trues and Brush] on Embankment None Animal Burrows and Washouts Damage to slopes or top of dam Cracked or Damaged Masonry Evidence of Seepage Evidence of Piping Erosion Leaks

12. Remarks & Recommendations: [Fully Explain]

In 1972 the Town of West Stockbridge completed extensive repairs on this dam.

At the time of this inspection, no deficiencies were noted.

1. Safe____X

2. Minor repairs needed___

3. Conditionally safe - major repairs needed___.

4. Unsafe_____.

5. Reservoir impoundment no longer exists [explain]

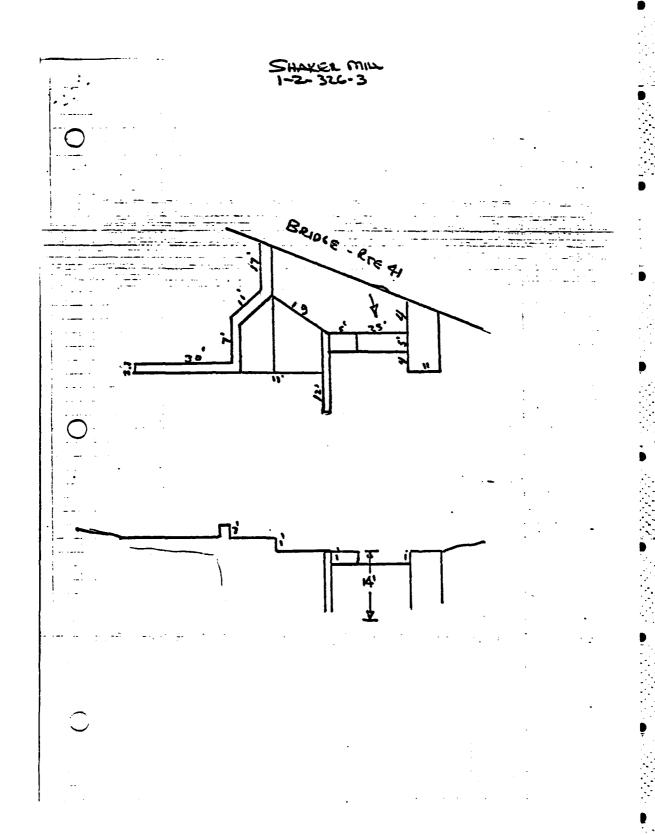
Recommend removal from inspection list_____.

... L-169

DESCRIPTION OF DAM

Submitted by RDJordan Dam No. 1-2-326-3 Date 1-18-73 City/Town West Stockbrid liams of Dam Shaker Mill Location: Topo Sheet No. 2-D Provide 8-1/2" x 11" in clear copy of tops map with location of D clearly indicated.	20
Location: Topo Sheet No. 2-D Provide 8-1/2" x 11" in clear copy of topo map with location of D	
Location: Topo Sheet No. 2-D Provide 8-1/2" x 11" in clear copy of topo map with location of D	
Location: Topo Sheet No. 2-D Provide 8-1/2" x 11" in clear copy of topo map with location of D	
Provide 8-1/2" x 11" in clear copy of tess map with location of D	
CISACIV INDICATIO	
Targetti in the second of the	em
Year built: 1910 . Year/s of subsequent repairs 1972	
Purpose of Dam: Mater Supply Recreational	
Irrigation . Other formerly power	
. Drainage Area:3_sq. mia	icres.
Normal Ponding Arca: 65 Acres; Avc. Depth	
Impoundment:gals;	
No. and type of dwellings located adjacent to pend or reservoir	
i.e. summer homes etc	- ,
Dimensions of Dam: Length85' . Hax. Height14'	
Slopes: Upstream Face conc.	
Counstream Face cone.	
Classification of Dam by Haterial:	
Cidadii idaa ii aa a	
Earth Conc. Masonry X . Stone Mas	sonry

	No. of people	Could cause severe damage to south West
· · · :	No. of homes	section of Town.
	- No. of Businesses	
	No. of Industries	Time
	No. of Utilities	Type
-	Rail mads	
•	Other dams	
	Cther	



160 160

INSPECTION REPORT - DAMS AND RESERVOIPS

Town of St Name Name Name Name Ilame Ilame O. of Pictures Regree of Hazard	Assessors Reg. of Deeds cockbridge St. & No. St. & No. St. & No. y] e.g. superinte by multi owners. St. & No. 1 if dam should	ndert, plant	Date of I Prev. Ins Pers. Con West St City/Town City/Town City/Town t manager, City/Town	State State State	MA Tel. N
Town of St Name Name Name Name Name Name Name Name Name or of Pictures Regree of Hazard	Reg. of Deeds cockbridge St. & No. St. & No. St. & No. y] e.g. superinte by multi owners. St. & No.	ndent, plant	Prev. Ins Pers. Con West St City/Town City/Town City/Town t manager, City/Town	state State State appointed by	MA: Tel. N: Tel. N: Tel. N: Absente
Town of St Name Name Name Name Name Name Name Name Name or of Pictures Regree of Hazard	Reg. of Deeds cockbridge St. & No. St. & No. St. & No. y] e.g. superinte by multi owners. St. & No.	ndent, plant	Pers. Con West St City/Town City/Town City/Town t manager, City/Town	State State State	MA e Tel. N e Tel. N e Tel. N e Tel. N
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aretaker [if and wher, appointed	y] e.g. superinte by multi owners. St. & No. taken 4	ndent, plant	t manager,	appointed by	absente
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o. of Pictures	taken 4	·		State	r Tel. N
egree of Hazard					
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	X			astrous	
This rating may	change as land u	se changes [ifuture dav	elopment]	
utlet Control:	Automatic		Manual 3	X.	•
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	3	. Pajor Rep	pairs	4. Urgent R	lepairs_
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_	Comment	Operative X Comments: Sourceam race of Dam: Condition 1	Operative X yes: Comments: Sourceam race of Dam: Condition: 1. Good X 3. Major Res	Operative X yes: Comments: Sourceam race of Dam: Condition: 1. Good X 3. Pajor Repairs	1. GoodX 2. Hinor Rs 3. Pajor Repairs 4. Urgent R

8			- 2 -		DAM NO. 1-2-326-3
	Downst	ream Face of Dam: Condition		. 2.	
					Urgent Repairs
		Comments:			
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<u> </u>	Friend	ency-Spillway+ Condition=	T cood	2 - Hipor	Romairs
•	Liller ga				Urgent Repairs
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11		ry of Deficiencies Noted:			
11	Summan	ry of Deficiencies Moted:	mbankment	NORIE	
11	Summa	Growth [Trees and Brush] on (
11	Summa	Growth [Trees and Brush] on [Animal Burrows and Washouts_			
11	Summar	Growth [Trees and Brush] on C Animal Burrows and Washouts_ Damage to slopes or top of do	np	n	
11	Summa	Growth [Trees and Brusk] on C Animal Burrows and Washouts_ Damage to slopes or top of do Cracked or Damaged Masonry_	<u> </u>	11	
11	Summa:	Growth [Trees and Brush] on [Animal Burrows and Washouts_ Damage to slopes or top of do Cracked or Pamaged Masonry_ Evidence of Suepage	<u> </u>	19 17 17 18	
11	Summa:	Growth [Trees and Brush] on [Animal Burrows and Washouts_ Damage to slopes or top of de Cracked or Damaged Masonry_ Evidence of Seepage Evidence of Piping	ır.	19 17 18 - 19	
11	Summa:	Growth [Trees and Brush] on [Animal Burrows and Washouts_ Damage to slopes or top of de Cracked or Damaged Masonry_ Evidence of Seepage_ Evidence of Piping_ Erosion	.m	19 17 18 19 18	
11	Summa:	Growth [Trees and Brush] on [Animal Burrows and Washouts_ Damage to slopes or top of do Cracked or Damaged Masonry_ Evidence of Suepage_ Evidence of Piping_ Erosion_ Leaks_		19 17 17 18 19	
11	Summa:	Growth [Trees and Brush] on [Animal Burrows and Washouts_ Damage to slopes or top of de Cracked or Damaged Masonry_ Evidence of Seepage_ Evidence of Piping_ Erosion	flov	19 17 17 18 19 11	

12. Remarks & Peconmendations: [Fully Explain] PREVIOUS INSPECTION DATE: 1/18/73

There were no deficiencies noted during this inspection. The concrete and 70 000 stone masonry structure appearshin good condition, no spalling or cracking is visible.

For location see Topo Sheet 2-D.

Overall Condition:

- 1. Safo______X_____.
- 2. Minor repairs needed______
- 3. Conditionally safe major recairs needed_____
- 4. Unsafe
- 5. Reservoir impoundment no longer exists [explain]

Recommend rumoval from inspection list_____



The Commonwealth of Massachusetts

EXECUTIVE OFFICE OF ENVIRONMENTAL AFFAIRS DEPARTMENT OF ENVIRONMENTAL QUALITY ENGR. DIVISION OF WATERWAYS

100 Nashua Sireet. Boston 0214

March 7, 1977

Board of Selectmen
Town of West Stockbridge
Town Hall
West Stockbridge, Mass. 01262

RE: Insp. Dam #1-2-326-3 Shaker Mill Dam West Stockbridge

Gentlemen:

On 11-4-76 , an Engineer from the Massachusetts Department of Public Works made a visual inspection of the above dam. Cur records indicate the owner to be Town of West Stockbridge.

If this information is incorrect will you please notify this office.

The inspection was made in accordance with the provisions of Chapter 253 of the Massachusetts General Laws as amended (Dars Safety Act). Chapter 705 of the Acts of 1975 transferred the jurisdiction of the so-called "Dams Safety Program" to the Commissioner of the Department of Environmental Quality Engineering.

The results of the inspection indicate that this dam is safe; however, the following conditions were noted that require attention:

1) Minor spalling of the gunite on spillway face.

We call these conditions to your attention before they become serious and more expensive to correct. With any correspondence please include the number of the Dam as indicated above.

Jehn J. Hannon, P E.

Chief Engineer

M'e:

Dean Amidon Robert Jordan Al McCallum File

S. L. L.

1.	Location: CDEW/	TOWN WEST STOCKBRID	<u> </u>	2-326-3
••	Name of Dam S	•	• • • • • • • • • • • • • • • • • • • •	by RDJordan-RSpaniol
	Name of cam	¥.	-	spection 11-4-76
		<u>. </u>		
2.	Cwner/s: per:	Assessors	rrev. Insi	pection_X
		Regof_Deeds	·	tact
	1 - Town of W	est Stockbridge	West Stockbridge	MA 01262
	Name	St. & No.	City/Town	State Tel
			City/Town	State Te
	Name	St. 2 No.	City/ torn	30000 10
	3	St. & No.	City/Town	State Tel. Ru
3.	Caretaker [if a owner, appointe	ny] e.g. superintend d by multi owners.		appointed by absented
	Hame	St. & 110.	City/Town	State Tel. No
4.	No. of Pictures	taken 1	·	
5.	Dogge of Maray	d: [if dam should fa	il completely]*	
				derate
				sastrous
		<u> </u>		•
	*This rating ma	ay change as land use	: changes [future da	
	Outlet Control	: Automatic	. Manual	
F 6.	Ogciec control		tyes:	
F 6.		000155146	•	
F 6.				
F 6.		nts:		
F 6.				
F 6.	- <u> </u>	nts:		
न्ह. -		of Dam: Condition	m:	
F 6.	- <u> </u>	of Dam: Condition	on: Cood	. 2. Utinor Repairs_
F 6.	upscream race	of Dam: Condition	ccod <u>x</u>	. 2. Hinor Repairs 4. Urgent Repairs

Emergency Spillway	/: Condition:	3. Major R	epairs4.	Urgent Ropai
Comments:	/: Condition:	3. Major R	epairs4.	Urgent Ropai
Emergency Spillway	v: Condition:	TEAT SUCCESSION		
Emergency Spillway	v: Condition:			
Emergency Spillway	v: Condition:			
Emergency Spillway	/: Condition:			
Emergency Spillway	/: Condition:			
Emergency Spillway	/: Condition:	3 0-1		
·			2. Minor F	erairs
·		3. Major Repai	rs4. l	Jrgent Repair:
Consider CS:				<u> </u>
•				
Mater level 9 time	of inspection:	<u>0.21</u> . ft.	abovex	below
		top of dam		
		principal sci	Nay X	 •
		other	.	<u> </u>
				
Summary of Deficie	encies Noted:			
Growth [Tree:	s and Brush] on E	mbankment	none	
Animal Eurre	es and Washouts			
	opes or top of da			
•	maged Nasonry			
	Suopage			
_				
	Piping		=-	
Leaks				
Trash and/or	debris immeding	flov <u> </u>		
	iocked spillway_			

L-158 B

DAM 110. 1-2-326-

2. Romarks & Percompandations: [Fu] by Explain PREVIOUS INSPECTION DATE: November 13, 1974

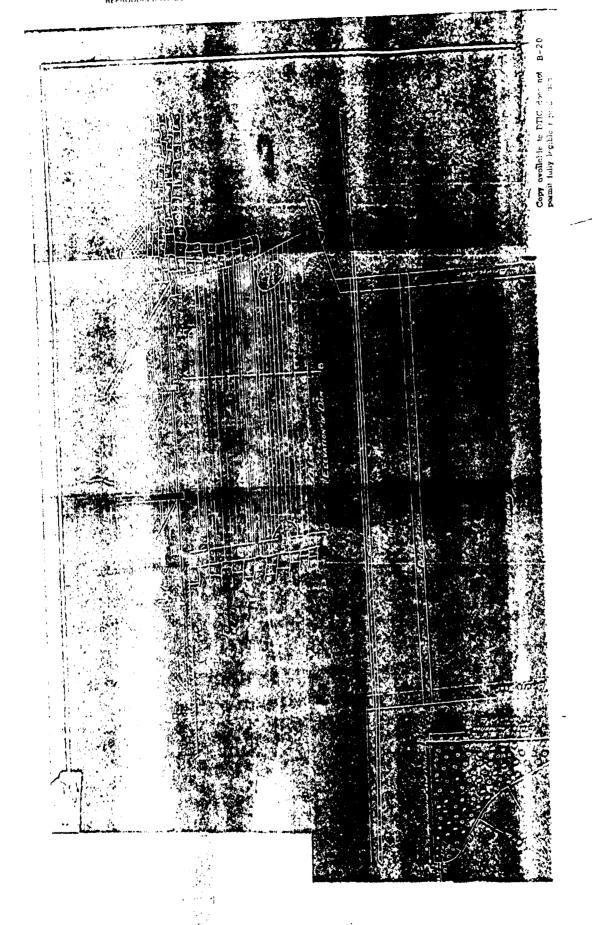
The only deficiency noted at this inspection was some minor spalling of the gumite on the spillway face. The abutments and the top of the dam are in good condition.

All drawdown equipment is functioning properly.

Por-location see-Tope Sheet-2-D.

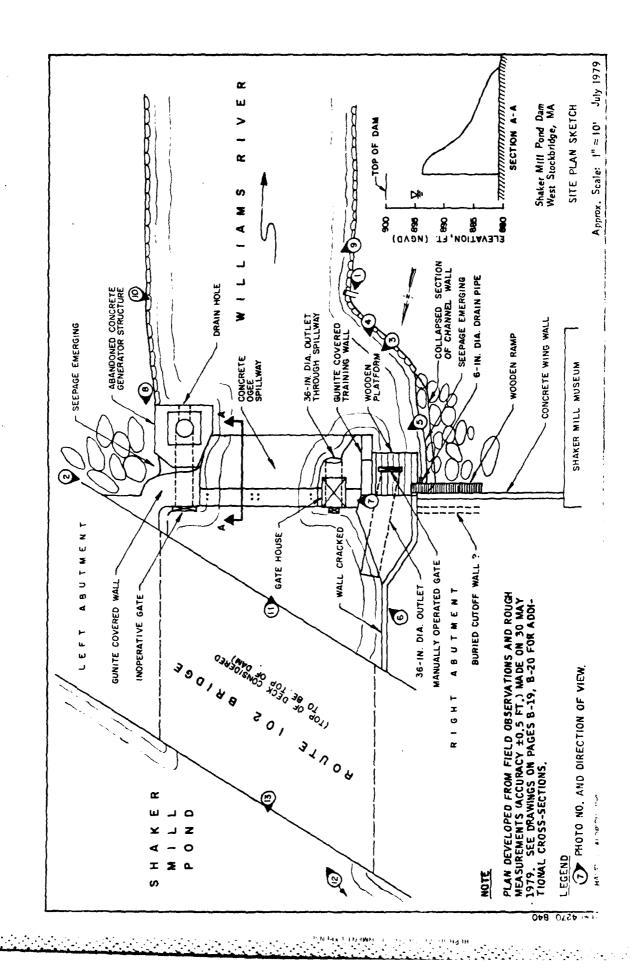
3. 0verall	Conditio	ाः स्ट्रिंग अस्ति ।
	1.	SafeX
٠.	2.	Minor repairs needed
	3.	Conditionally safe - major repairs needed
	1.	Unsafe
	5.	Reservoir impoundment no longer exists [explain]
·		Recommend removal from inspection list





APPENDIX C - PHOTOGRAPHS

				Page		
LOCA	TION PLAN					
Site Plan Sketch						
PHOT	OGRAPHS					
No.	<u>Title</u>	<u>Roll</u>	Frame	Page		
1.	Overview of Shaker Mill Pond Dam	C39	1	vi		
2.	Spillway and right approach channel wall	17	11	C-2		
3.	Spillway, center outlet through spillway and left approach channel walls	17	7	C-2		
4.	Right outlet works and wing wall at right abutment	17	5	C-3		
5.	Deteriorated right spillway training wall	17	23	C-3		
6.	Upstream side of dam	C39	12	C-4		
7.	Center outlet gate control mechanism inside gate house	C39	18	C-4		
8.	Gunite covered wall and rock fill at left abutment where seepage is emerging	17	17	C-5		
9.	Abandoned concrete generator structure and left discharge channel wall	17	4	C-5		
10.	Collapsed first 20 ft. of right discharge channel wall	17	13	C-6		
11.	Downstream channel below dam (April 1979)	A1	16A	C-6		
12.		17	8	C-7		
13.	Shaker Mill Pond upstream from Route 102 bridge	17	25	C-7		

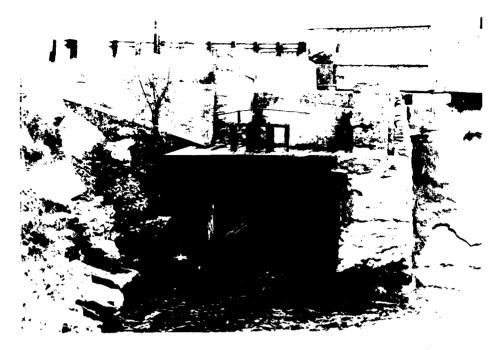




2. Spillway and right approach channel wall



 Spillway, center outlet through spillway and left approach channel walls



 Right outlet works and wing wall at right abutment



5. Deteriorated right spillway training wall



6. Upstream side of dam



 Center outlet gate control mechanism inside gate house



 Gunite covered wall and rock fill at left abutment where seepage is emerging



9. Abandoned concrete generator structure and left discharge channel wall



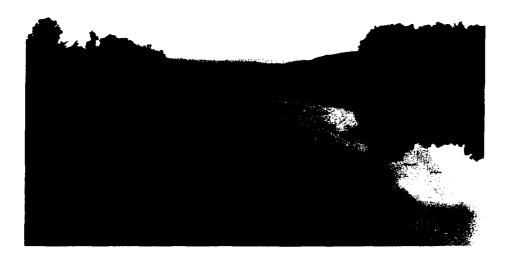
10. Collapsed first 20 ft. of right discharge channel wall



11. Downstream channel below dam (April 1979)



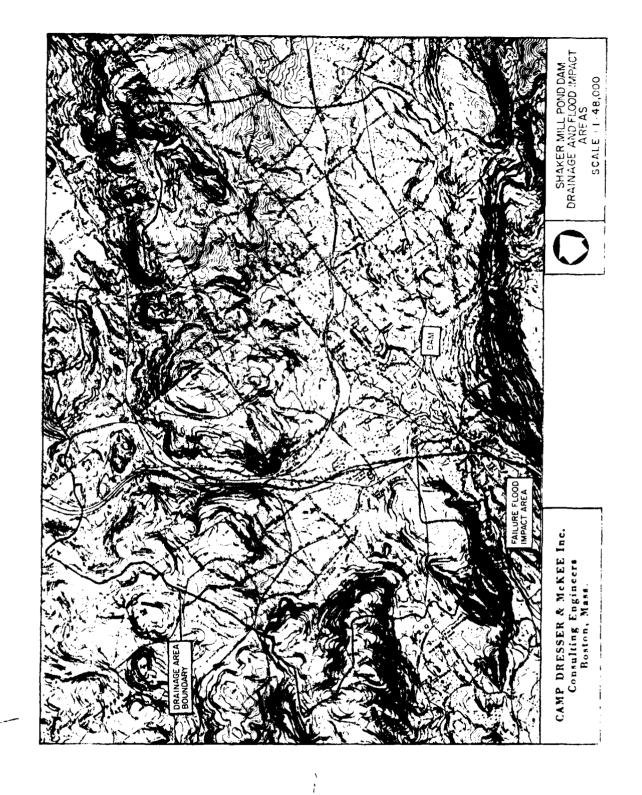
12. Upstream side of Route 102 bridge structure



13. Shaker Mill Pond upstream from Route 102 bridge

APPENDIX D - HYDROLOGIC AND HYDRAULIC COMPUTATIONS

	Page
Subject	
Drainage Area and Failure Flood Impact Area Map Size Classification, Hazard Potential and Test	D-1 D-2
Flood Development Surcharge-Storage Routing, Tail Water Stage-Discharge Curve, Dam and Spillway	D-3 D-4
Pond Area-Volume Curve Stage-Discharge Curve, Tailwater	D-5 D-6
Capacity of Existing Spillway	D-7
Dam Failure Analysis Hydraulic Profiles (Before and After Failure)	D-8 D-9
Downstream Channel Cross-Sections and Stage-Dis- charge Relations	D-11



AMP DRESSER & McKEE Environmental Engineers Boston, Mass.	CLIENT HYA JOB NO 561-9-R+-14 PAGE / PROJECT COE Dam Inspection DATE CHECKED 7/2/79 DATE 6/18/79 DETAIL SHAKER MILL FOND DAM CHECKED BY RHS COMPUTED BY ALL
Si	28 Classification
Da	m Height = Els. : 900.1 - 879.7 = 20.4-Ft (40-Ft.
Sł	orage Volume: 1,200 ac-ft @ E1. 900.1 _> 1,000 ac-f
	Size: Intermediate
Наз	ard Potential Classification
In sub	case of a dam failure the right bank would be ject to flooding, particularly in the area downstram. Depot street. The hazard pokenhal is considered "high" were of potential for loss of lives and excersive idential and commercial property demagn.
Te	st Flood Development
	e: Intermediate <u>Hazard Potential</u> : High
Test	Flood Flows PMF
Wal	ershed . Area: 32.4 sqmi = 20,736 acres
Tel	rain = rolling with 5 percent flat (wake, swamps, etc.)
Per	k Flow Rate: 1250 cfs/sqmi
PA	1F = 32.4 = 1250 = 40,500 cfs = Spillway Test Flood Inflow
	- I

Surcharge = Storage Routing WIFE = Pand = 926 = Sur stage discharge curre in Page D-40) Band Storage Valume = 19,200 as th (See Roma Valume curre), page D-5) Narmal Pond Valume = 130 as th (See Roma Valume curre), page D-5) Narmal Pond Valume = 130 as th (See Roma Valume curre), page D-5) STOR = (13,205-120) to 11,04 -in STOR = 5,570-112 3,45 -im	OFFICE A MARKET MG.	CLIENT,		H = A)		J	38 NO.	561-9)-R+-	14	PAGE.		
Surcharge = Storage Routing Gan = A0,500 cfs							ATE CHI	ECKED.	7/2/29			DATE.		_
Gq = A0,500 cfs (PRE - Mar Runnell 19") WSE = Pand = 926 0 (See stage discharge curre in Page D-4) Bond Storage Valume = 19,200 as-4t (See Brea-Valume runner page D-5) Normal Pand Valume = 13,00 as-4t (See Brea-Valume runner page D-5) Normal Pand Valume = 1300 as-4t (See Brea-Valume runner page D-5) Normal Pand Valume = 1300 as-4t (See Brea-Valume runner page D-5) Normal Pand Valume = 13,00 as-4t (See Brea-Valume runner page D-5) Normal Pand Valume = 130,000 as-4t (See Brea-Valume runner page D-5) STDR = 5,5970:12 3,05 sin		DETAIL	SHAKER	MILL	POND D	9 /4	CHECK	ED SY			COMP	ITED BY	AUE	
Gap = 40,500 cfs (PAF = Mass Remost 19") WSE = Pand = 926 0 (See stage discharge curve in Page D=4) Bond Storage Valume = 19,200 as-it (See Brea-Valume runner, page D=5) Normal Pand Valume = 7 (30 as-it G E) , 893.8 STDR = (13,289-120)12 11,04 = in 20,736 19 16,970 cfs WSE (Send) = 911 AV & SIDU-DOZ 53 STDR 2 = 5,970-12 = 3,45 = in STDR 3 = 5,970-12 = 3,45 = in STDR	· · · · · · · · · · · · · · · · · · ·		ì			-1			·					
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WSE = Pand = 926			ļ				·		<u> </u>	<u>; i </u>			·	
WSE = Pand = 926		<u>·</u>	 	-				· .	<u> </u>	+ 	 			
Road Storage Volume: 19,200 ac-ft (see Area-Volume views, page 0-5) Normal Pond Volume: - 130 ac-ft (P El. 893.8 STDR: (13,200-170) 12 11.04 - 111 32,715 32,715 32,50 cft WSE (Good) = 91/1 AV = 6100-170=53 STDR: 2,5370:12 3,45 cin STDR: -7.75 Op. 25,030 cft STDR: 6,42 Op. = A0,500 (1 - 6.07) = 2(,800 cft STDR: 6,42 Op. = A0,500 (1 - 6.07) = 2(,800 cft STDR: 6,42 Op. = A0,500 (1 - 6.07) = 2(,800 cft STDR: 6,42 Op. = A0,500 (1 - 6.25) = 27,200 cft WSE (food) = 318.0 AV = 10,800 ac-ft STDR: 6,28 STDR: 6,28 STDR: 6,28 STDR: 6,28 STDR: 6,28 STDR: 6,28 TEST FLOOD OUT FLOW: 27,200 cft Q food Fl. 918.0 Tail Water The tailwake stage dicharge curve on page P=6 shows that the spillway crest would be submerged by about 18.8 feet (912.6 - 893.8) at the dest flood dicharge	(3)	= 40,5	00 ch_	LIME	4	the K	re-eff	- 19	*) ;				! : :	
Road Storage Valume: 19,200 ac-ft (See Brea-Valume curry, page 0-5) Normal Pond Valume: - 130 ac-ft (P El. 893.8 STDR (13,200-170) 12 11.04 - 11 30,736 19			 			++	+++	! 					 	
Normal Pand Valume = 130 ac-ft @ E . 893.8 57DR (15,285-130)12 ,04 - 20,736 20,736 ,04 - 57DR 2 5,970-12 3,45 - 20,736 57DR 2 7,25 57DR 2 5,970-12 3,45 - 20,736 57DR 2 7,25 57DR 2 5,970-12 3,45 - 57DR 2 5,901-12 3,45 - 57DR 2 5,43 57DR 2 5,43 57DR 2 5,43 57DR 2 6,43 57DR 2 6,43 57DR 2 6,43 57DR 2 6,43 57DR 2 6,28 57DR 3 6,28 57DR 3 6,48 57DR 3 6,48 57DR 4 57DR 4 57DR 4 57DR 4 57DR 4 57DR 5 57DR 5 57DR 5 57DR 5 57DR 5 57DR 6 57DR 6 57DR 6 57DR 6 57DR 6 57DR 6 57DR 7 57DR 7	- INSI	<u> </u>	d	926	- See	ونطع	e dist	horge	curve	Lin_	Page_	D-4)	 	
Normal Pand Valume = 130 ac-ft @ E . 293.8 57DR (15,200-130)12 ,04 - 20,736 20,736 57DR 2,5370-12 3,45 - 57DR 20,736 AV = 9,700 57DR 2,561 57DR 6,43 Qp = 40,500 (1 - 6,42) 2 (1,800 cft) 16 and wife = 317.7 AV = 10,500 ac-ft 57DR 6.08 57DR 6.25 16 and wife = 317.7 AV = 10,500 ac-ft 57DR 6.08 57DR 6.25 17 and wife = 317.7 AV = 10,500 ac-ft 57DR 6.08 57DR 6.25 TEST Flood OUT Flows 27,200 cft G fond El. 218.0 Tail Water The tailwaler stage-discharge curve en page D=6 5 hours Hat the spillway crest would be submerged by about 18.8 feet (912.1 - 832.8) at the sent flood discharge 18 about 18.8 feet (912.1 - 832.8) at the sent flood discharge 19 about 18.8 feet (912.1 - 832.8) at the sent flood discharge 19 about 18.8 feet (912.1 - 832.8) at the sent flood discharge 10 about 18.8 feet (912.1 - 832.8) at the sent flood discharge 10 about 18.8 feet (912.1 - 832.8) at the sent flood discharge 10 about 18.8 feet (912.1 - 832.8) at the sent flood discharge 10 about 18.8 feet (912.1 - 832.8) at the sent flood discharge		, (1	- 3/.1			- i	11 /	-	-	,	-			-
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STOR 1	Non	mal P	nd Val	-	- /3	0 0	1-4	0	El. s	202.8				
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STOR 2 = 5.570:12 = 3.45 - im														
STOR 2 = 5.570:12 = 3.45 - im	G.	- 40.50	0/1-11	04	16.970	och		WSE	(Pand)	= 91	1	AV= 6	100-130=	5,9
WE = Cond = 216.6 AV = 9.700 STOR = 5.61° STOR = 6.43° QP = 40.500 (1 - 6.42) = 26.800 cfs. Cond wsE = 217.7 AV = 10.500 ac.p. STOR = 6.08 STOR = 6.25° Op = 40.500 (1 - 6.23) = 27.200 cfs wsE (cond) = 318.0 AV = 10.850 a STOR = 6.28" ≈ 6.25" TEST FLOOD OUT FLOW = 27.200 cfs Q Cond Fl. 218.0 Tail Water : The tailwater stage discharge curre on page 0-6 shows that the spillway crest would be subverged by about 18.8 feet (312.6 - 832.8) at the test flow discharge														
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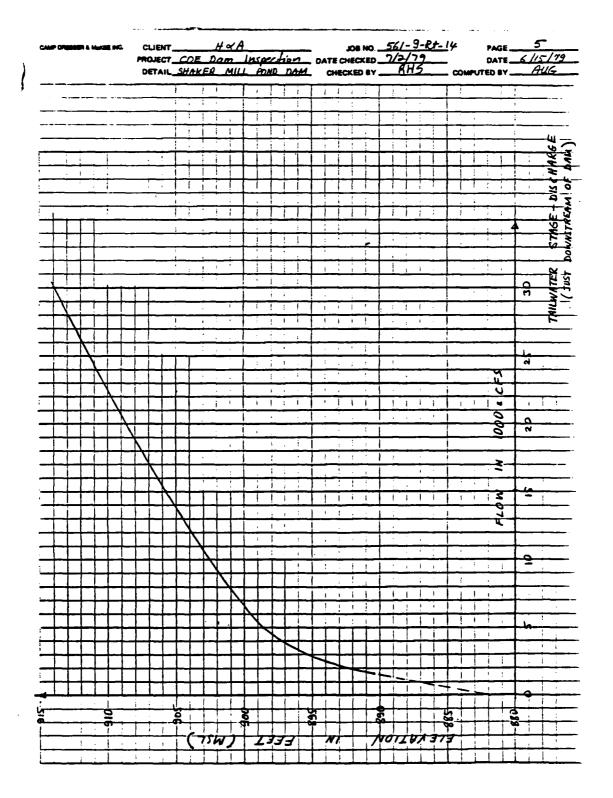
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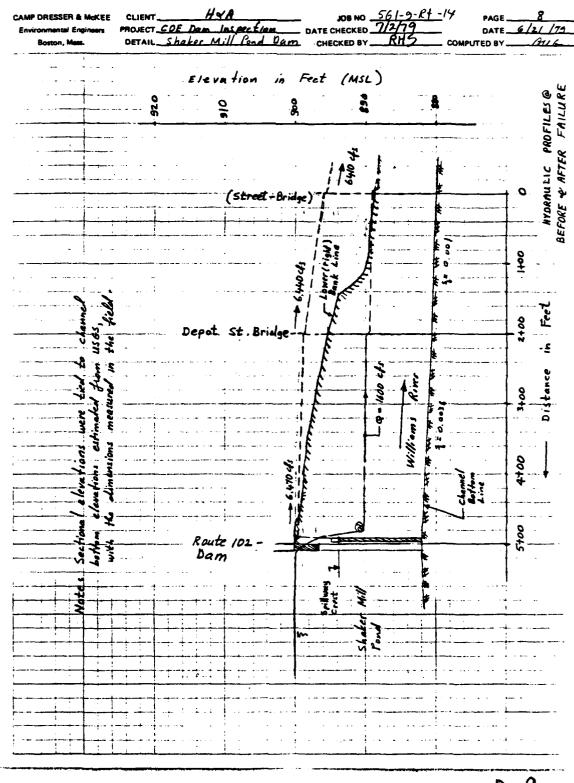
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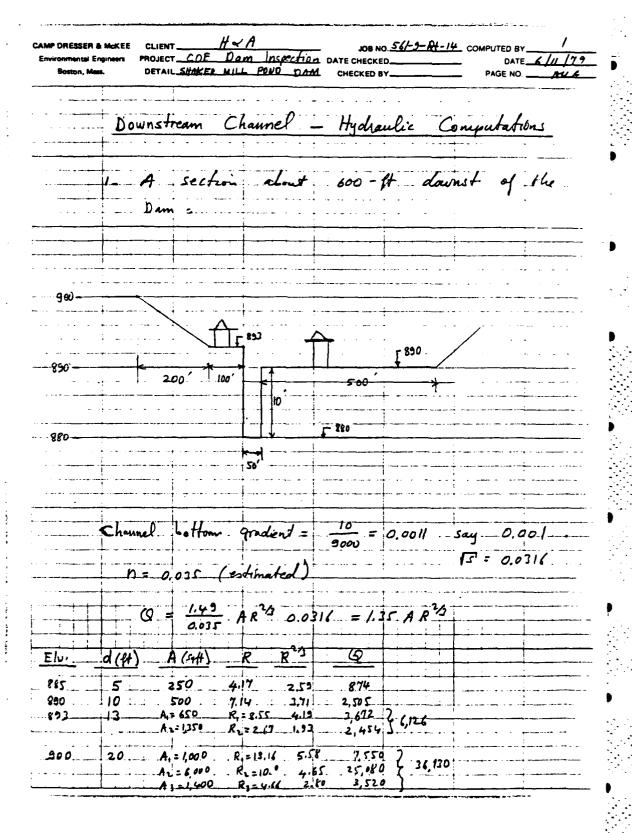
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JOB NO _ 56/- 9-Rt-14 $H \propto A$ CLIENT DATE 6/21 /74 PROJECT COE Dam Inspection DATE CHECKED 7/2/79 DETAIL SHAKER MILL POND DAM CHECKED BY Dam Failure Analysis Estimata : W = 985 × 49.2 = 41.8 4. 20.4 QP = \$.41.8.567.92.1 = 6470 cfs Storage Volume @ E. 301.1 1200 ac-ft. Approximate hydraulic are shown in Page D-9. Flood Flow Routing : between Depot St. 5 Dam Op @ Depot St = Op (1-V1 = 357+1175 200= 356 = 5.3 ac-st · (negligible amount) Op = 6,470 (1 - 5.1) = 6,440 41 5=0,0022 (From Mousins; A=705 R14 6; WEST_STOCKERINGE Ah = 0.6 - ft. ne 0035) WSE @ Depot_st. Reach 2 MILL POND WILLIAMS V3 = 1,160 + 1240 = 200 = 1 = 55 act OP = 6,440 (1- 5.5) = 6,410 ds **≈ 300** The lower reach (Reachs) would 4-ft (downstream of Dept St.) to 7-ft (upstream of the second budge)



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APPENDIX E - INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS

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